Multi-Objective Optimization of Machining Parameters for Multi-Pass CNC Turning to Minimize Carbon Emissions, Energy, Noise and Cost

Bening Maulina Fittamami*, Eko Pujiyanto, Yusuf Priyandari

Abstract: Global warming is a huge environmental issue today. This is due to the high level of world carbon emissions. The manufacturing process accounts for 30% of the world's carbon emissions production. Sustainable manufacturing is necessary to implement to reduce carbon emission levels caused by the manufacturing process. There are three aspects of sustainable manufacturing, namely environmental aspects, economic aspects, and social aspects. These three aspects can be implemented in the machining process by optimizing machining parameters in multi-pass CNC turning. This research aims to optimize CNC turning machining parameters by considering energy consumption, carbon emissions, noise, and production cost. The model is solved using a Multi-objective Genetic Algorithm in Matlab 2016b then the transformation and weighting functions are carried out from the feasible value. Based on the optimization results, the total energy consumption value obtained is 2.50 MJ; total production cost is $ 2.19; total carbon emissions are 5.97 kgCO2, and noise is 236, 19 dB. The sensitivity analysis exhibits the machining parameters that affect the objective function: The cutting speed parameter and the feed rate parameter. This model can be used to improve the manufacturing process and support sustainable manufacturing.

Keywords: Sustainable manufacturing, multi-objective optimization, energy, cost, carbon emissions, noise.

Introduction

The manufacturing industry plays a vital role in the global economy. However, it also causes various problems due to energy consumption, environmental sustainability, and personal health [1]. For example, the manufacturing industry sector accounts for 50% of total energy consumption [2]. Global warming is the most significant environmental issue today due to high carbon emissions. The manufacturing process accounts for 30% of the world's carbon emissions. Energy consumption in manufacturing has increased twofold over the past 60 years, and the number continues to grow [3].

Global warming has prompted the formation of policies related to the earth's climate change. Kyoto Protocol is one of the policies issued by the UNFCCC [4] in 1990. The aim of the Kyoto Protocol is to reduce carbon emissions of each country by 52% from 1990 levels. Several countries have implemented carbon emission taxes as a form of commitment to the Kyoto Protocol. Due to this policy, the manufacturing industry has new challenges to reduce production costs. Therefore, the manufacturing industry needs to adapt by implementing sustainable manufacturing. Sustainable manufacturing is creating manufactured products to minimize negative impacts on the environment, energy-saving, and natural resources, and are safe for employees, society, and consumers. There are three aspects of sustainable manufacturing: economic, environmental, and social [5]. This research developed an optimization model of multi-pass CNC turning by considering energy consumption, carbon emissions, production cost, and noise.

Previous research such as [6, 7, 8, 9] stated that machining parameters such as cutting speed, feed rate, and depth of cut can affect the energy and costs incurred during machining. Arif, et al. [10] developed an energy optimization model consisting of machining, idle, tool replacement, and cutting tool energy. Chen and Tsai [11] minimized the production cost per unit with machining components, machine idle, tool replacement, and tool costs. The carbon emissions model uses the model proposed by Li et al. [3], total carbon emissions consist of electricity, cutting tool chip carbon emissions, cutting fluid carbon emissions, and material chip carbon emissions, cutting fluid carbon emissions, and material carbon emissions. The development of the noise model is based on the research conducted by Cirtu
The method used in this research is a Genetic Algorithm. A Genetic Algorithm is a computational algorithm that can be used to solve the search for optimal solutions in a more natural optimization [13, 14]. In this method, the solution step begins with coding to represent the real problem into biological terminology. Then, individuals who can proceed to reproduction were selected. A Crossbreeding is used to produce children from two chromosomes and mutations to make changes to a gene or individual [15]. The mathematical model of the objective function of energy consumption, carbon emissions, noise, and production cost was optimized using the Genetic Algorithm Method in the MATLAB R2016b software with two times the amount of rough. From this method, a feasible solution is obtained for the optimization of the objective function.

Furthermore, the results of the feasible solution were processed using the transformation function method. Problems with multi-objective optimization can be solved using a transformation function [16]. The transformation function is used to equalize the different units into dimensionless units. After obtaining a dimensionless value, the Weighted Sum Method was applied. The WSM score is obtained by multiplying the given weight score by the objective function score [17]. The amount of weight was adjusted to the decision maker’s preference, which represents the relative importance of the objective function. Here is an equation of the Weighted Sum Method (WSM).

\[ U = \sum_{i=1}^{k} w_i f_i(x) \]  

(1)

**Decision Variable**

The object of this research is multi-pass machining of CNC Turning, which will be optimized by considering energy consumption, carbon emission, noise, and production cost. The decision variables of this study are cutting speed of roughing, cutting speed of finishing, roughing feed rate, finishing feed rate, depth of cut in roughing, and depth of cut in finishing (see Table 1 as a comparison).

**List of Notations**

\[ C_{Elec} \] : Electricity carbon emissions (kgCO₂)
\[ C_{tool} \] : Cutting tool carbon emissions (kgCO₂)
\[ CEF_{Elec} \] : Electricity carbon emission factor (kgCO₂/kWh)
\[ CEF_{tool} \] : Cutting tool carbon emissions factor (kgCO₂/kWh)
\[ C_m \] : Machining cost ($) 
\[ C_i \] : Machine idle cost ($) 
\[ C_r \] : Tool replacement cost ($) 
\[ C_{ru} \] : Tool cost ($) 
\[ E_c \] : Machining energy (MJ) 
\[ E_i \] : Idle energy (MJ)
$E_r$ : Tool replacement energy (MJ)
$E_T$ : Tool energy (MJ)
$D$ : Diameter of workpiece (mm)
$L$ : Length of workpiece (mm)
$C_{\text{opt}}, p, q, r$ : Constant related tool life
$apr_{\text{max}}$ : Upper bound of depth of rough cut (mm)
$apr_{\text{min}}$ : Lower bound of depth of rough cut (mm)
$aps_{\text{max}}$ : Upper bound of depth of finish cut (mm)
$aps_{\text{min}}$ : Lower bound of depth of finish cut (mm)
$f_r_{\text{max}}$ : Upper bound of feed rate in rough machining (mm)
$f_r_{\text{min}}$ : Lower bound of feed rate in rough machining (mm)
$f_s_{\text{max}}$ : Upper bound of feed rate in finish machining (mm)
$f_s_{\text{min}}$ : Lower bound of feed rate in finish machining
$u_r_{\text{max}}$ : Upper bound of cutting speed in rough machining (m/min)
$u_r_{\text{min}}$ : Lower bound of cutting speed in rough machining (m/min)
$u_s_{\text{max}}$ : Upper bound of cutting speed in finish machining (m/min)
$u_s_{\text{min}}$ : Lower bound of cutting speed in finish machining (m/min)
$h_1, h_2$ : Constants pertaining to tool travel and approach/depart time (min)
$k$ : Specific cutting energy (J/m$^3$)
$k_0$ : Direct labor cost and overhead ($/\text{min}$)
$k_t$ : Cutting edge cost ($$/\text{edge}$)
$k_1, k_2, k_3$ : Constants for roughing and finishing parameter relations
$k_q$ : Chip tool interface temperature constraint
$k_f$ : Constraint in surface roughness
$P_0$ : Idle power (kWh)
$P_t$ : Tool power (MJ/insert)
$R_r_{\text{max}}$ : Upper bound of surface roughness in roughing (µm)
$R_s_{\text{max}}$ : Upper bound of surface roughness in finishing (µm)
$re$ : Nose radius of tool (mm)
$V$ : Volume rate of material removal ($m^3$/min)
$te$ : Tool replacement time (min/edge)
$tp$ : Preparation time (min/unit)
$tm$ : Machining time (min)
$t_{mr}$ : Machining time of roughing (min)
$t_{ms}$ : Machining time of finishing (min)
$tl$ : Idle time (min)
$tc$ : Variable time (min)
$T$: Tool life of roughing and finishing (min)
$T_{ri}$ : Tool life of i-th roughing (min)
$T_s$ : Tool life finishing (min)
$W_{\text{tool}}$ : Mass of tool
$w$ : Weight
$Q_{ri}$ : Chip tool interface temperature during roughing (°C)
$Q_s$ : Chip tool interface temperature during finishing (°C)
$Q_{u}$ : Maximum allowable chip-tool interface temperature (°C)
$F_{ri}$ : Cutting force during roughing (kgf)
$F_s$ : Cutting force during finishing (kgf)
$F_{\text{max}}$ : Maximum allowable cutting force (kgf)
$\delta, \phi, \tau$ : Constants related to equation of chip tool interface temperature
$\mu, \theta$ : Constants related to cutting force
$\eta$ : Machine efficiency
$i$ : Possible value of roughing pass

### Machining Time

Machining time is the time used during the machining process. Machining time significantly affects the energy consumption used during machining and the total production cost. Time in the turning process is divided into four types: machining time, idle time, tool wear time, and tool replacement time. The equation for the machining time ($tm$) is formulated as follows:

$$tm = tm_r + tms$$  \hspace{1cm} (2)

$t_{mr}$ is the time needed during roughing and $t_{ms}$ is the time needed during the process. The roughing process was carried out several times. The roughing and finishing time are formulated as follows,

$$tm_r = \sum_{i=1}^{n} \frac{\pi DL}{1000 v_{fsf_i}}$$  \hspace{1cm} (3)

where, $D$ is diameter workpiece and $L$ is length of workpiece.

$$tms = \frac{\pi DL}{1000 v_{fsf}}$$  \hspace{1cm} (4)

Total machining time [10,11]

$$tm = \sum_{i=1}^{n} \frac{\pi DL}{1000 v_{fsf_i}} + \frac{\pi DL}{1000 v_{fsf}}$$  \hspace{1cm} (5)

The equation of idle time is divided into two parts, namely the time during loading and unloading operations ($t_p$). $t_p$ score is constant. $t_c$ is the tool idle motion when it approaching/departing the edge of the workpiece. The equation of idle time is provided as follows

$$t_i = t_p + t_c$$  \hspace{1cm} (6)

Equation of idle time when the tool approaches arrives at the workpiece ($t_c$)

$$t_c = n(h_1L + h_2) + (h_1L + h_2)$$  \hspace{1cm} (7)
Total idle time
\[ t_i = t_p + \left( n(h_1L + h_2) + (h_1L + h_2) \right) \] (8)

Tool life equation is expanded using Taylor’s equation and can be formulated as follows
\[ vT^{a}f^{b}ap^{γ} = C \] (9)
\[ T = \frac{c^{1/a}}{vT^{a}f^{b}ap^{γ}/a} = \frac{c_{0}}{vT^{a}f^{b}ap^{γ}} \] (10)

Assumed that the entire machining process used the same tools for roughing \((T_{ri})\) and finishing process \((T_{s})\). Between roughing and finishing process, there is differens wear rate of tools due to different machining condition. Therefore, \(T\) can be contracted as the summation of those two processes.
\[ T = \theta T_{ri} + (1 - \theta)T_{s} \] (11)
\[ T_{ri} = \frac{vT^{a}f^{b}ap^{γ}}{c_{a}a_{p}r_{i}} \] (12)
\[ T_{s} = \frac{c_{a}a_{p}r_{s}}{vT^{a}f^{b}ap^{γ}/a} \] (13)

Energy Consumption

The total energy consumption \((E_{\text{total}})\) in the machining process of multi-pass turning is obtained from the machining energy consumption \((E_{c})\), energy consumption when the machine is idle \((E_{i})\), energy consumption when replacing tools \((Em)\) and energy consumption of tools \((Et)\) based on the optimization model developed by Arif et al. [10].

Energy consumption in machining \((E_{c})\)

Energy consumption in machining \((E_{c})\) is the energy used during the machining process for material feeding. The amount of energy consumption is determined by idle power, feeding volume, and length of machining time or as formulated as follow.
\[ E_{c} = (Po + kV)tm \] (14)

where, \(Po\) denotes idle power, \(k\) is the machining specific energy, \(V\) is the feeding volume and \(tm\) is the machining time.

Energy consumption at idle \((E_{i})\)

When the machine is idle, the energy required is the same as the energy when there is no spindle rotation.
\[ E_{i} = Po \times tl \] (15)

Using equation (8) and (15) the idle time can be written as
\[ E_{i} = Po \times \left( tp + n(h_1L + h_2) + (h_1L + h_2) \right) \] (16)

Energy consumption when replacing tool

The cutting tool is replaced when the engine is running but the spindle is turned off. According to Shaw [19], the part-by-part tool replacement time is the result of the time of tool replacement per edge with the total edge consumed \((tm/T)\).
\[ Em = Po \times te \left( \frac{tm}{T} \right) \] (17)

Cutting tool energy consumption

According to Shaw [19], the part-by-part tool replacement time is the result of the tool replacement time per edge with the total of the consumed edge.
\[ Et = Pt \times \left( \frac{tm}{T} \right) \] (18)

Total carbon emissions

Total energy is the sum of machining energy, energy when the machine is idle, energy when replacing tools, and cutting tool energy.
\[ E_{\text{total}} = Ec + El + Em + Et \] (19)

The equation for the total energy can be simplified by categorizing it into the total energy during roughing and finishing. They can be formulated as follows:
\[ E = \left( (Po + kV) + \frac{P_{\text{oxf}t}}{T} + \frac{P_{\text{oxf}r}}{T} \right) (tm) + (Po \times tl) \] (20)
\[ Es = \left( (Po + kV) + \frac{P_{\text{oxf}t}}{T_{s}} + \frac{P_{\text{oxf}r}}{T_{s}} \right) (tm) + (Po \times tc) \] (21)
\[ Er = \left( (Po + kV) + \frac{P_{\text{oxf}t}}{T_{ri}} + \frac{P_{\text{oxf}r}}{T_{ri}} \right) (tm) + (Po \times tc) \] (22)
\[ E = Ec + \sum_{i=1}^{n} Er + (Po \times tp) \] (23)

Carbon Emissions

The optimization model in the research conducted by Li et al. [3] provided total carbon emissions in the machining process of turning consisting of electricity carbon emissions, cutting tool carbon emissions, cutting fluid carbon emissions, material carbon emissions, and speck carbon emissions. The model developed in this research is dry turning condition machining. Therefore, cutting fluid is not required. According to Yi et al. [20], material carbon emissions and carbon emissions only have a minimal effect on machining parameters. Thus, they are not included in the optimization model of carbon emissions.
\[ CE = CE_{\text{elec}} + CE_{\text{tool}} \] (24)

Electricity carbon emissions \((CE_{\text{elec}})\)

The amount of carbon emissions of CNC machine that comes from electricity is determined by the amount of the electric carbon emission factor and the total energy consumption during machining process.
\[ CE_{\text{elec}} = CE_{\text{elec}} \times E_{\text{total}} \] (25)
\[ CE_{elec} = CEF_{elec} \times \left( E_s + \sum_{i=1}^{n} E_r + (Po \times tp) \right) \] (26)

CEF_{elec} may vary in each region. This is due to differences in the structure of the electrical network. In this research, the CEF_{elec} rate is 0, 6747 kgCO2/kWh, in line with the national average of electric carbon emission factors. This CEF_{elec} data is quoted from the Ministry of National Development and Reform Commission (NDRC) of China.

Cutting tool carbon emissions (CE_{tool})

The amount of carbon emission for cutting tools can be obtained by multiplying the ratio of machining time on tool life expectancy with the carbon emission factor of cutting tools and the mass of cutting tools.

\[ CE_{tool} = \frac{tm}{T} \times CEF_{tool} \times W_{tool} \] (27)

CEF_{tool} is the carbon emission factor of cutting tool and W_{tool} is the mass of cutting tool. Based on the research conducted by Rajemi and Matievenga [21], on manufacturing process, the carbon emission factor for cutting tool is 29.6 kgCO2/kg.

Total carbon emissions

The total carbon emissions generated during the manufacturing process are the sum of electricity carbon emissions and cutting tool carbon emissions. Total carbon emissions is formulated as follows

\[ CE = CEF_{elec} \times \left( E_s + \sum_{i=1}^{n} E_r + (Po \times tp) \right) + \frac{tm}{T} \times CEF_{tool} \times W_{tool} \] (28)

Noise

The objective function of noise represents the social aspect of sustainable manufacturing as personal health. Noise must remain on the safe threshold. Thus, it is crucial to develop acceptable machining models. In Cirtu’s [12], the noise model is still in the form of single-pass turning. Then, this research will be developed into multi-pass turning.

\[ N = \sum_{i=1}^{n} N_{ri} + N_s \] (29)

\[ N_{ri} = \sum_{i=1}^{n} \left( a \times Po + b \times \left( \frac{fr}{f_{ri}} \right) + c \times \left( Po \times \left( \frac{fr}{f_{ri}} \right) \right) + Lm \right) \] (30)

\[ N_s = a \times Po + b \times \left( \frac{fr}{f_{sa}} \right) + c \times \left( Po \times \left( \frac{fr}{f_{sa}} \right) \right) + Lm \] (31)

Production Costs

According to Chen and Tsai [11], production costs in the machining process of multi-pass CNC turning can be divided into four cost elements, namely machining cost (Cm), idle cost or cost during machine preparation and tool setting (Ci), tool replacement cost (Ctr), and tool wear cost (Ctw).

\[ C = Cm + Ci + Ctr + Ctw \] (32)

Machining cost

Machining cost is the result of multiplying direct labor costs and overhead (ko) with machining time (tm).

\[ Cm = ko \times tm \] (33)

\[ Cm = k_0 \times \left( \sum_{i=1}^{n} \frac{nDL}{1000v_s f_i} + \frac{nDL}{1000v_s f_s} \right) \] (34)

Idle cost

There are two times of idle time, namely loading and unloading operation constant time and variable time [22]. The idle process occurs during tool preparation and cutting tool settings. The following is the equation for idle machine cost.

\[ Ci = ko \times tt \] (35)

\[ Ci = ko \times [tp + (n(h_1L + h_2) + (h_1L + h_2))] \] (36)

Tool replacement cost

Tool replacement cost is the multiplication of direct labor cost and overhead (ko) with the time to replace the tool.

\[ Ctr = ko \times (te(t_m/T)) \] (37)

Tool wear cost

Tool wear cost is the cost incurred during the tool usage. kt is the cost of each cutting edge.

\[ Ctw = kt \times (t_m/T) \] (38)

Total production cost per unit

The total production cost per unit is the sum of machining cost, idle cost, tool replacement cost, and tool wear cost. The following is the equation for the total production cost.

\[ C = (ko \times tm) + (ko \times tt) + (ko \times te(t_m/T)) + (kt \times (t_m/T)) \] (39)

Constraints

Constraints in roughing:

Cutting speed in roughing

\[ v_{rmin} \leq v_r \leq v_{rmax} \] (40)

Depth of cut in roughing.

\[ f_{rmin} \leq f_r \leq f_{rmax} \] (41)

Feed rate in roughing

\[ a_{rmin} \leq a_{fr} \leq a_{frmax} \] (42)
Cutting force constraint in roughing
\[ F_r = k_f f_r^2 a_p \leq F_{max} \]  
(43)

Cutting power constraint in roughing
\[ P_r = k_f f_r^2 a_p \frac{v_r}{6000} \leq P_{max} \]  
(44)

Chip tool interface temperature constraint
\[ Q_s = k_q V_r f_r^\phi \frac{a_p}{d_p} \leq Q_u \]  
(45)

Constraint in surface roughness
\[ f_r \leq \sqrt{\frac{r_p F_{max}}{32.1}} \]  
(46)

Constraints in finishing:
Cutting speed in finishing
\[ v_{s_{min}} \leq v_s \leq v_{s_{max}} \]  
(47)

Depth of cut in finishing
\[ f_{s_{min}} \leq f_s \leq f_{s_{max}} \]  
(48)

Feed rate in finishing
\[ a_{ps_{min}} \leq a_{ps} \leq a_{ps_{max}} \]  
(49)

Cutting force constraint in roughing in finishing
\[ F_s = k_f f_s^2 a_p \leq F_{max} \]  
(50)

Cutting power constraint in finishing
\[ P_s = k_f f_s^2 a_p \frac{v_s}{6000} \leq P_{max} \]  
(51)

Chip tool interface temperature constraint
\[ Q_s = k_q V_s f_s^\phi \frac{a_p}{d_p} \leq Q_u \]  
(52)

Constraint in surface roughness
\[ f_s \leq \sqrt{\frac{r_p F_{max}}{32.1}} \]  
(53)

The relation of roughing and finishing parameters
Relation of cutting speed parameters
\[ v_s \geq k_1 f_r \]  
(54)

Relation of feed rate parameters
\[ f_r \geq k_2 f_s \]  
(55)

Relation of depth of cut parameters
\[ a_{ps} \geq k_3 a_{ps} \]  
(56)

Total depth of cut
\[ a_p = a_p + \sum a_{ps} \]  
(57)

Results and Discussions

Numerical Example and Analysis

Numerical examples are taken from previous studies with adjustments based on the context of the problem (model) that has been created in this research. The workpiece used in this study has a diameter of 50 mm and a length of 300 mm. The total depth of the cut is 6 mm. The maximum cutting power is 5 kW, and the maximum cutting force is 1960 Newton. The maximum temperature on the workpiece surface is 1000°C. The maximum surface roughness in the roughing process is 25 µm, and the maximum surface roughness in the finishing process is 2.5 µm. The mechanical efficiency (\(\eta\)) is 85%. Table 2—Table 6 exhibit the parameter setting for the numerical analysis.

Result

The search for the solution of this research model was carried out in two stages, particularly using the Genetic Algorithm method with Matlab R2016b
software and using the transformation and weighting functions for each objective function. The Genetic Algorithm is used to determine the feasible solution value of the objective function, namely cost minimization, energy minimization, noise minimization, and carbon emission minimization. The genetic algorithm scheme is depicted in Figure 1. In this research, there are two roughing processes and one finishing process.

Through feasible solution value (see Table 7), the optimal value can be obtained with normalization by using transformation and weighting function procedures. Each objective function has a weighted value of 0.25 according to the importance level of the objective function.

The result of multi-objective optimization shown in (Table 8) with total production cost of $2,19\,$; total energy consumption is 2,50 MJ; total noise of 236,19 dB; and total carbon emission of 5,97 kgCO₂.
The purpose of the sensitivity analysis in this research is to show the behaviour of the model parameters in some model parameters, namely feed rate in roughing process ($f_{r1}$), feed rate in finishing process ($f_{s}$), cutting speed in roughing ($v_{r1}$) and the cutting speed in finishing ($v_{s}$). All of the machining parameters are chosen as the decision variables, and $n$ equal to 2. Various experiment sets were designed for analysis. All experiment are shown in Table 9.

### Table 7. Feasible minimum and maximum value used for the normalization stage

<table>
<thead>
<tr>
<th>Decision Variable</th>
<th>$C_{total}$ ($)</th>
<th>$E_{total}$ (MJ)</th>
<th>$N_{max}$ (dB)</th>
<th>$C_{total}$ (kgCO2)</th>
</tr>
</thead>
<tbody>
<tr>
<td>$f_s$</td>
<td>0.28</td>
<td>0.10</td>
<td>0.29</td>
<td>0.11</td>
</tr>
<tr>
<td>$aps$</td>
<td>0.82</td>
<td>1.15</td>
<td>1.17</td>
<td>1.21</td>
</tr>
<tr>
<td>$vs$</td>
<td>303.20</td>
<td>72.92</td>
<td>273.33</td>
<td>53.41</td>
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<tr>
<td>$fr_2$</td>
<td>0.88</td>
<td>0.26</td>
<td>0.90</td>
<td>0.25</td>
</tr>
<tr>
<td>$fr_3$</td>
<td>0.39</td>
<td>0.26</td>
<td>0.34</td>
<td>0.29</td>
</tr>
<tr>
<td>$fr_4$</td>
<td>0.63</td>
<td>0.63</td>
<td>0.89</td>
<td>0.41</td>
</tr>
<tr>
<td>$apr_2$</td>
<td>2.63</td>
<td>2.41</td>
<td>2.44</td>
<td>2.48</td>
</tr>
<tr>
<td>$apr_3$</td>
<td>1.64</td>
<td>1.65</td>
<td>1.63</td>
<td>1.63</td>
</tr>
<tr>
<td>$apr_4$</td>
<td>1.27</td>
<td>1.28</td>
<td>1.25</td>
<td>1.26</td>
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<tr>
<td>$v_{r2}$</td>
<td>82.29</td>
<td>53.15</td>
<td>70.55</td>
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<tr>
<td>$v_{r3}$</td>
<td>61.69</td>
<td>55.15</td>
<td>79.13</td>
<td>55.44</td>
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<td>$v_{r4}$</td>
<td>167.56</td>
<td>167.59</td>
<td>75.66</td>
<td>70.66</td>
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### Table 8. Optimization result

<table>
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<tr>
<th>Objective function</th>
<th>Unit</th>
<th>Value</th>
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<tbody>
<tr>
<td>Production cost</td>
<td>$</td>
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<tr>
<td>Energy consumption</td>
<td>MJ</td>
<td>2.50</td>
</tr>
<tr>
<td>Noise</td>
<td>dB</td>
<td>236.19</td>
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<tr>
<td>Carbon emission</td>
<td>kgCO2</td>
<td>5.97</td>
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<table>
<thead>
<tr>
<th>Decision variable</th>
<th>Unit</th>
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<tr>
<td>Feed rate in finishing ($fs$)</td>
<td>mm/rev</td>
<td>0.27</td>
</tr>
<tr>
<td>Depth of cut in finishing ($aps$)</td>
<td>mm</td>
<td>0.93</td>
</tr>
<tr>
<td>Cutting speed in finishing ($vs$)</td>
<td>mm/minute</td>
<td>308.09</td>
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<tr>
<td>Feed rate in roughing ($fr_1$)</td>
<td>mm/rev</td>
<td>0.84</td>
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<tr>
<td>Depth of cut in roughing ($apr_2$)</td>
<td>mm</td>
<td>2.55</td>
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<tr>
<td>Cutting speed in roughing ($vr_2$)</td>
<td>mm/minute</td>
<td>78.08</td>
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<td>Roughing pass</td>
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<table>
<thead>
<tr>
<th>Objective function value ($U$)</th>
<th>Value</th>
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<tbody>
<tr>
<td></td>
<td>0.013</td>
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### Table 9. Sets of parameters

<table>
<thead>
<tr>
<th>Control parameter</th>
<th>Values</th>
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<tbody>
<tr>
<td>$fr_1$</td>
<td>[0.84; 1.48; 2.11; 2.74; 3.37]</td>
</tr>
<tr>
<td>$fr_2$</td>
<td>[0.84; 1.48; 2.11; 2.74; 3.37]</td>
</tr>
<tr>
<td>$fs$</td>
<td>[0.27; 0.47; 0.54; 0.67; 0.74]</td>
</tr>
<tr>
<td>$vr_1$</td>
<td>[78.08; 136.64; 195.20; 253.76; 312.32]</td>
</tr>
<tr>
<td>$vr_2$</td>
<td>[78.08; 136.64; 195.20; 253.76; 312.32]</td>
</tr>
<tr>
<td>$vs$</td>
<td>[308.09; 539.17; 616.19; 770.24; 781.95]</td>
</tr>
<tr>
<td>$apr_1$</td>
<td>[2.55; 2.45; 2.35; 2.25; 2.15]</td>
</tr>
<tr>
<td>$apr_2$</td>
<td>[2.55; 2.45; 2.35; 2.25; 2.15]</td>
</tr>
<tr>
<td>$aps$</td>
<td>[0.93; 0.83; 0.74; 0.65; 0.56]</td>
</tr>
</tbody>
</table>

### Sensitivity Analysis

The purpose of the sensitivity analysis in this research is to show the behaviour of the model parameters in some model parameters, namely feed rate in roughing process ($fr_1$), feed rate in finishing process ($fs$), cutting speed in roughing ($vr_1$), and the cutting speed in finishing ($vs$). All of the machining parameters are chosen as the decision variables, and $n$ equal to 2. Various experiment sets were designed for analysis. All experiment are shown in Table 9.
consumption, production costs, and carbon emissions increase when the feed rate and cutting speed in roughing process increase. However, in the noise objective function, changes in the feed rate and cutting speed of the roughing process do not significantly affect the noise value. When the parameter values in the finishing process increase, the value of energy consumption, production costs, and carbon emissions will decrease, meanwhile, the noise objective function is not significantly affected by changes in the finishing feed rate parameters and finishing cutting speed.

From figure 4, it can be seen that changes in the depth of cut parameter have only a small effect on the results of the three objective functions (production costs, carbon emissions, and noise). In the energy consumption objective function, the value increases when the feed rate in roughing process parameter is increased. The value of the carbon emission objective function increases slightly when the feed rate in roughing process parameter is increased.

It can be inferred that changes in parameters are sensitive to the three objective functions. Conversely, the noise objective function is insensitive to changes in parameters. This is because the machining parameters only have a minimal effect on the value of the noise objective function. Meanwhile, in the other three objective functions, machining parameters have a big influence. Thus, optimizing the machining parameters is necessary to minimize the level of carbon emission, energy consumption, and high production cost. Based on the sensitivity analysis results, the machining parameters can affect the four objective functions. The manufacturing industry must keep attention to the use or choice of machining parameters to support sustainable manufacturing.

### Conclusion

This research produces a multi-objective optimization model that can optimize machining parameters to minimize production cost, energy consumption, noise, and carbon emission. The machining parameters considered in this research are cutting speed, depth of cut, and feed rate in each roughing and finishing process. This research is the optimal value of each machining parameter. The total energy consumption value obtained is 2.50 MJ; total production cost is $219; total carbon emissions are 5.97 kgCO2, and noise is 236.19 dB.

Based on the sensitivity analysis results, the machining parameters that affect the objective function are the cutting speed parameter and feed rate parameter. However, changes in machining parameters do not have a significant effect on the noise objective function. This research can be improved in various directions. Further research can add tool wear conditions. Thus, it can be adjusted to a real CNC turning system.

### References


